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ADVANCED NAVAL VEHICLE CONCEPTS EVALUATION (ANVCE) SHIP ACCELER--ETC(U)

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Item 0001AA

Working Paper
August 1976

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Advanced Naval Vehicle Concepts Evaluation

(ANVCE) SHIP ACCELERATION LIMITS

N00167-76-M-8390

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DECLASSIFICATION STATEMENT A

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SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM										
1. REPORT NUMBER W.P. No. 196-8	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER										
4. TITLE (and Subtitle) ANVCE Ship Acceleration Limits (U)		5. TYPE OF REPORT & PERIOD COVERED										
		6. PERFORMING ORG. REPORT NUMBER										
7. AUTHOR(s)		8. CONTRACT OR GRANT NUMBER(s) N00167-76-M-8390										
9. PERFORMING ORGANIZATION NAME AND ADDRESS Payne, Inc. Annapolis, Maryland 21401		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS										
11. CONTROLLING OFFICE NAME AND ADDRESS CNO (OP96V) Washington, D.C. 20350		12. REPORT DATE August 1976										
		13. NUMBER OF PAGES 6										
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)		15. SECURITY CLASS. (of this report) Unclassified										
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE										
16. DISTRIBUTION STATEMENT (of this Report) Unlimited and approved for Public release.												
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)												
18. SUPPLEMENTARY NOTES												
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) Advanced Naval Vehicle Concepts Evaluation ANVCE Technology Assessment Acceleration Limits Ride Quality of Naval Vehicles												
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) The purpose of this note is to define the tolerable acceleration limits for vehicles in the ANVCE study. In decreasing order of severity, these limits are: <table border="0"> <tr> <td>Limit</td> <td>Physiological Description (Experienced Navy Crew):</td> </tr> <tr> <td>(A)</td> <td>Severe, less than one hour;</td> </tr> <tr> <td>(B)</td> <td>Tolerable, less than one hour;</td> </tr> <tr> <td>(C)</td> <td>Long-term, severe;</td> </tr> <tr> <td>(D)</td> <td>Long-term, tolerable.</td> </tr> </table>			Limit	Physiological Description (Experienced Navy Crew):	(A)	Severe, less than one hour;	(B)	Tolerable, less than one hour;	(C)	Long-term, severe;	(D)	Long-term, tolerable.
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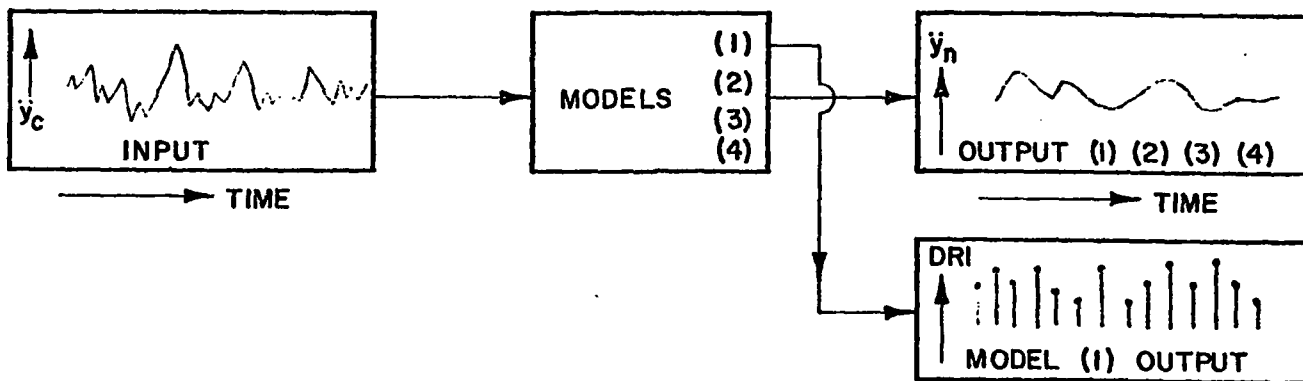
ANVCE SHIP ACCELERATION LIMITS

The purpose of this note is to define the tolerable acceleration limits for vehicles in the ANVCE study. In decreasing order of severity, these limits are:

<u>Limit</u>	<u>Physiological Description (Experienced Navy Crew)</u>
(A)	Severe, less than one hour
(B)	Tolerable, less than one hour
(C)	Long-term, severe
(D)	Long-term, tolerable

One would normally design to meet limits (B) and (D), accepting the more severe conditions (A and C) for only a small percentage of the total operational profile, or if very substantial advantages (such as greatly reduced cost, perhaps) accrue from operation at the more severe limit.

The physiological effect of the vehicle's acceleration time history (\ddot{y}_c) for a given set of operating conditions is assessed by exciting (or "driving") four dynamic models with it, and observing the model output (\ddot{y}_n).



The basic model equation is as follows

$$\ddot{\delta} + 2\bar{c}\omega_n \dot{\delta} + \omega_n^2 \delta = \ddot{y}_c$$

$$\ddot{y}_n = \ddot{y}_c - \ddot{\delta}$$

where δ is the deflection of the spring of a simple sprung mass model, ω_n (rad/sec) is the natural frequency of the model, and \bar{c} is the damping ratio.

<u>Model Number</u>	<u>\bar{c}</u>	<u>ω_n (rads/sec)</u>	<u>Name</u>
①	0.224	52.9	Spinal
②	0.40	25.1	Visceral
③	1.0	52.9	Body Vibration
④	1.0	1.571	Low Frequency

The VIBRATION RIDE QUALITY INDEX (VRQI) is defined as

$$VRQI = \frac{\ddot{y}_n' \text{ (RMS)}}{g}$$

where $\ddot{y}_n' \text{ (RMS)}$ is the maximum value obtained from one of the four model outputs.

The limits on VRQI are as follows:

<u>Limit</u>	<u>Description</u>	<u>VRQI must be less than:</u>
A	Severe, less than one hour	0.5
B	Tolerable, less than one hour	0.2
C	Long term, severe	0.2
D	Long term, tolerable	0.1

The IMPACT RIDE QUALITY INDEX (IRQI) is obtained from the "DRI" output of Model Number ①, the "spinal model."

$$DRI = \frac{\omega_1^2 \delta_1 \text{ MAX}}{g}$$

$\delta_1 \text{ MAX}$ is computed for each maximum value; i.e. each δ_1 when $\dot{\delta}_1 = 0$, $\ddot{\delta}_1 < 0$

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We now order the DRI values as in the following example:

<u>DRI</u>	<u>Number of Occurrences/hr.</u>	<u>DRI Exceedance Point</u>	<u>Number of Exceedances/hr.</u>	<u>Corresponding Number of Exceedances in 24 hrs.</u>
0 -0.5	109	0	149	3576
0.5-1.0	9	0.5	40	960
1.0-1.5	10	1.0	31	744
1.5-2.0	7	1.5	21	504
2.0-2.5	7	2.0	14	336
2.5-3.0	4	2.5	7	168
3.0-3.5	2	3.0	3	72
3.5-4.0	1	3.5	1	24
4.0-4.5	0	4.0	0	0
4.5-5.0	0	4.5	0	0

The exceedances per twenty-four hours are obtained by ratioing up from the duration for which readings were actually obtained; in this example, one hour. The exceedance points are then plotted as shown ("Example A") in Figure 1. The IRQI is defined as the largest value which occurs. In Example A, IRQI = 1.0, so that the ride is just at the limit of tolerability. In Example B, the maximum value is about IRQI = 0.38, indicating a relatively smooth ride.

Reference

1. Payne, P.R.

"On Quantizing Ride Comfort and Allowable Accelerations." Paper to be Presented at the 3rd Advanced Naval Vehicles Conference, Arlington, Virginia (September 1976).

